

Ignition of Hydrogen-Air Mixtures by Moving Heated Particles

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Caltech



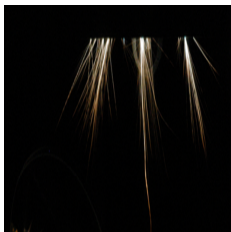
Outline

- 1 Motivation
- 2 Previous Work
- 3 Goal
- 4 Physical Model, Numerical Approach and Simulation Parameters
- 5 Results
- 6 Discussion
- 7 Closing Remarks

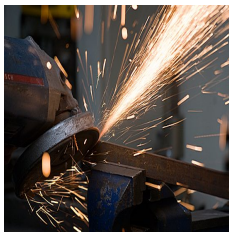
Motivation - Why is it important ?

Motivation

Improved understanding of ignition hazards



Aircraft fuel tank safety¹



Manufacturing safety²



Mining safety³

-
1. Simulated lightning strike on composite coupon performed at Boeing
 2. Mechanical sparks from cutting and reshaping processes
 3. Hot particles of decomposed explosive and casing

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Experimental work

Classical Experimental Work

In the 1930's motivated by coal-mining operations - frictional sparks (moving heated particles)

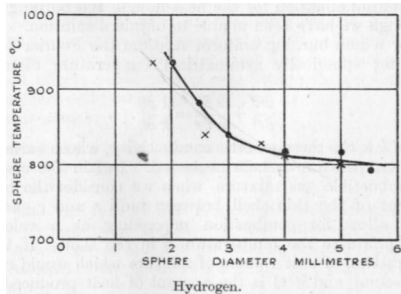


Figure 5 : effect of particle diameter¹

1. R.S. Silver. *Phil. Mag. J. Sci.*, 23(156) : 632-657/1937.

Experimental work

More Recent Experimental Work

Ignition of gaseous mixtures by submillimeter size stationary hot particles

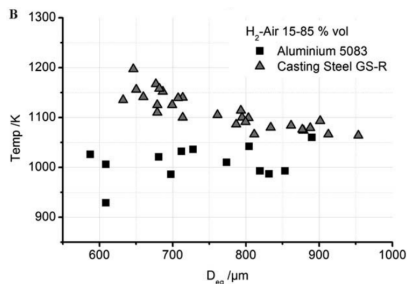


Figure 2b : effect of particle material²

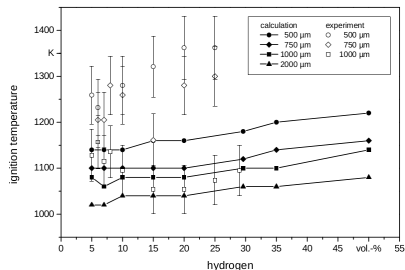


Figure 4 : effect of mixture concentration³

2. D. Roth et al. *Combust. Sci. Techno.*, 186 :10-11/2014.

3. M. Beyer and D. Markus. *8th ISHPMIE Yokohama, Japan*, 2010.

Experimental work

Previous & Current Experimental Efforts at Caltech

Ignition of *n*-hexane mixtures

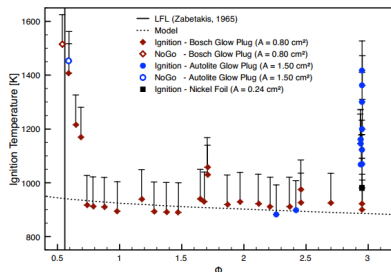


Figure 3.15 : transiently heated surfaces ⁴

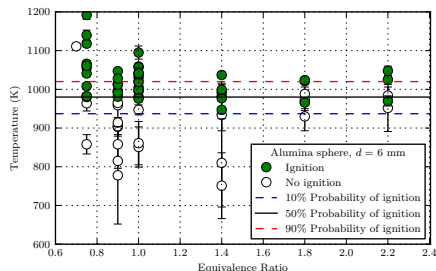


Figure : moving heated spheres ⁵

4. P.A. Boettcher. *Ph.D Thesis. Caltech*, 2012.

5. S. Coronel. *Ph.D Thesis. Caltech (in preparation)*, 2015.

Numerical work

Some Previous & Current Numerical Efforts

1D Simulation assuming spherical symmetry, quiescent atmosphere and no-thermally induced convection

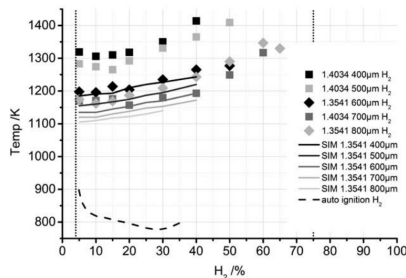


Figure 3b : Effect of mixture concentration ⁶

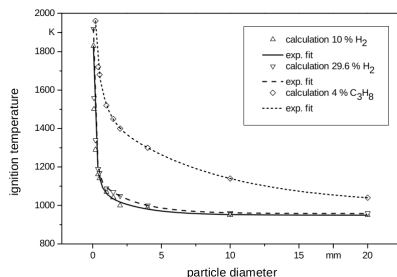


Figure 8 : Effect of particle size ⁷

6. D. Roth et al. *Combust. Sci. Techno.*, 186 :10-11/2014.

7. M. Beyer and D. Markus. *8th ISHPMIE Yokohama, Japan*, 2010.

Theoretical Work

Analysis

- C.K. Law⁸ - Stagnation-point ignition of a premixed combustible and ignition of a combustible by hot particles (B.L. equations, one-step irreversible reaction and high activation energy limit)
- Y. B. Zel'dovich⁹ - Ignition of a fuel mixture flowing around an object (B.L. equations, one-step irreversible reaction, Dorodnitsyn transformation, no assumptions made w.r.t. activation energies, complete analytical investigation of the system was impossible)
- More recently Golovin, A.M. and Golovin, A.M & Rudakova, N.B.¹⁰ with similar simplifying assumptions ...

8. *Int. J. Heat Mass Transfer.*, 21 : 1363-1368/1978a. ; *AIAA Journal*, 16(6) :628-630/1978b.

9. *The Mathematical Theory of Combustion and Explosions*, 1985.

10. *High Temperature*, 1996/1998.

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Goal

Objective

- Explain the dynamics of ignition of combustible gases by inert moving heated spheres when close and far from the ignition limit
- Study the competition between diffusive and convective losses, and chemical heat release to unravel the complex physics and chemistry at play within the boundary layer during the ignition process
- Explore the quantitative prediction of ignition thresholds

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Physical Model - Governing Equations

Reactive Navier-Stokes with temperature dependent properties
 (μ : Sutherland Law, $\alpha = k/c_p$: Eucken Relation, c_p : JANAF)

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{u}) = 0$$

$$\frac{\partial(\rho \mathbf{u})}{\partial t} + \nabla \cdot (\rho \mathbf{u} \mathbf{u}) = -\nabla p + \nabla \cdot \tau + \rho \mathbf{g}$$

$$\frac{\partial(\rho h)}{\partial t} + \nabla \cdot (\rho \mathbf{u} h) = \nabla \cdot (\kappa/c_p \nabla h) + q_{chem}, \quad (Le = 1)$$

$$\frac{\partial(\rho Y_i)}{\partial t} + \nabla \cdot (\rho \mathbf{u} Y_i) = \nabla \cdot (\rho D_i \nabla Y_i) + \Omega_i$$

with $p = \rho \bar{R}T$, $\tau = (p + \frac{2}{3}\mu \nabla \cdot \mathbf{u})\mathbf{I} + \mu[\nabla \mathbf{u} + (\nabla \mathbf{u})^T]$

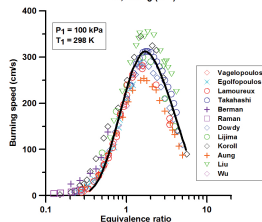
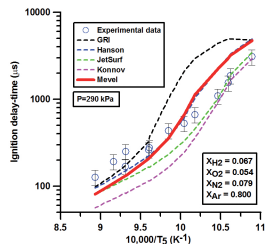
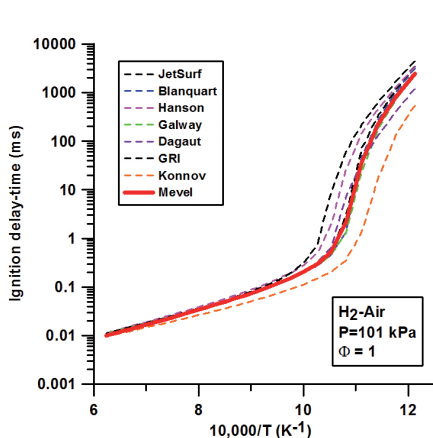
$$h = \sum h_i Y_i, \quad q_{chem} = \sum h_i \Omega_i, \quad \Omega_i = \rho dY_i/dt$$

Challenges

- Wide range of temporal and spatial scales involved
 - Size of experimental apparatus ($\mathcal{O}(m)$)
 - Hydrodynamic length scales - Boundary layer thickness ($\mathcal{O}(\mu m) - \mathcal{O}(mm)$)
 - Chemical induction/ignition times ($\mathcal{O}(s)/\mathcal{O}(ms)$) and flame thickness ($\mathcal{O}(\mu m)$)
- Size of detailed chemical kinetic mechanisms
 - Hydrocarbon fuels conventionally used for transportation comprise thousands of reactions and hundreds of species (e.g. *n*-hexane detailed mechanism : 2581 reactions and 457 species)

Physical Model - Hydrogen Chemistry

Mével's Mechanism (9 species and 21 reactions)¹¹



11. R. Mével et al. *P. Combust. Inst.*, 32 & 33 / 2009 & 2011

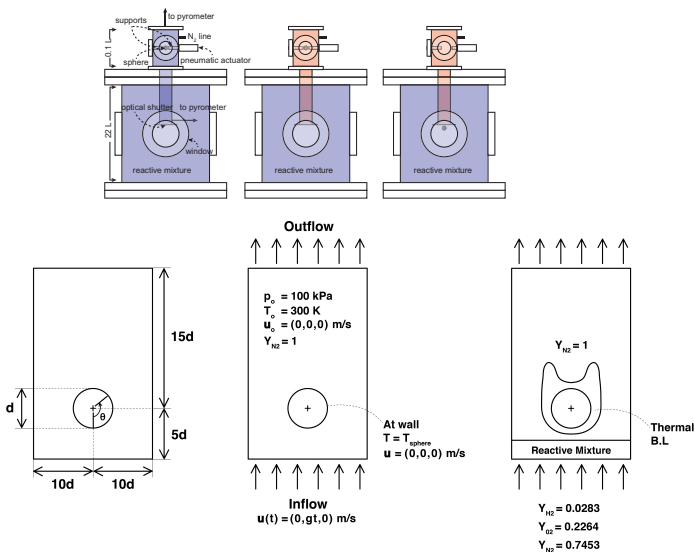
Approach

- 2D simulation of reactive viscous flow using the Open source Field Operation And Manipulation (OpenFOAM) toolbox ¹²
- Spatial discretization done with Finite Volumes (FV)
- Pressure-velocity coupling achieved using PIMPLE (PISO + SIMPLE) ¹³
- Implementation of time dependent boundary conditions to reproduce actual experimental conditions
- High Performance Computing - resources provided by the Extreme Science and Engineering Discovery Environment (XSEDE) supported by the National Science Foundation (NSF)

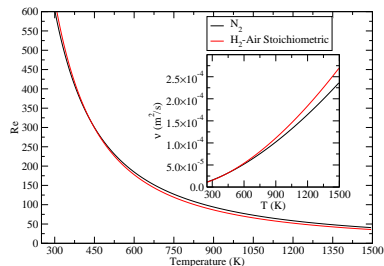
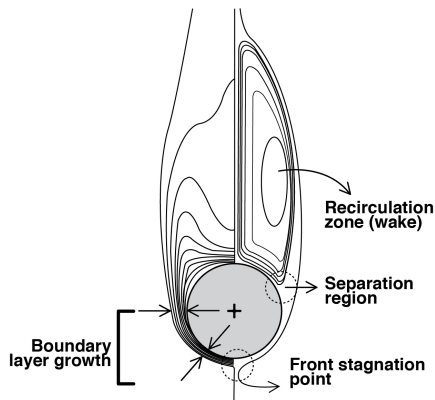
12. H.G. Weller et al. *J. Comput. Phys.*, 12 : 620-631/1998.

13. I. Demirdzic and Péric. *Int. J. Numer. Meth. Fl.*, 16 : 1029-1050/1993.

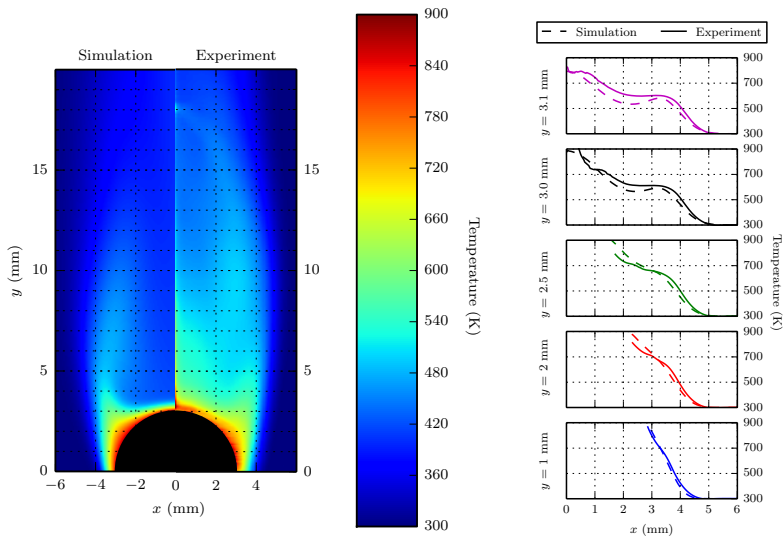
Experimental setup, initial & boundary conditions



Nature of flow before contact with reactive mixture



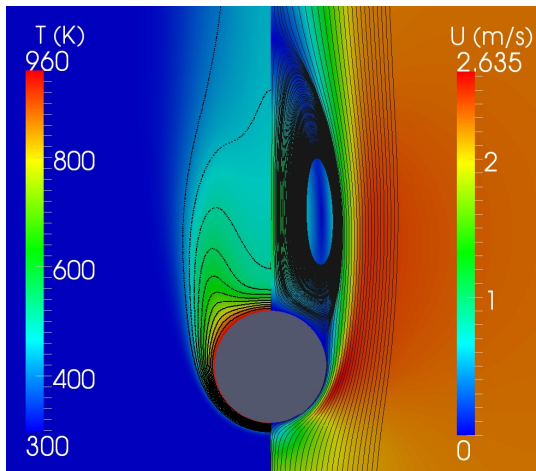
Comparison with non-reactive experiments



Outline

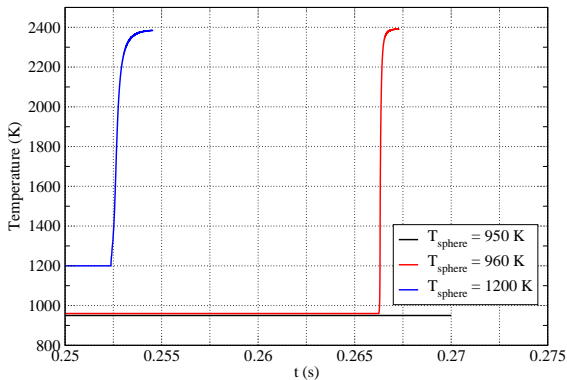
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Flow structure - boundary layer development



Temperature and velocity fields, temperature isocontours and streamlines before contact with reactive mixture

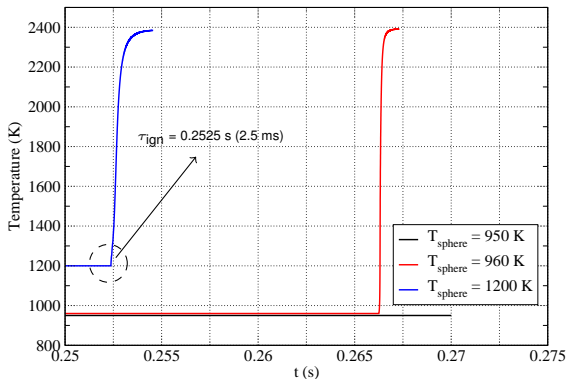
When does ignition take place ?



Temperature maximum in computational domain

$$\tau_{\text{ign}} = T_{\text{sphere}} + 150\text{K}$$

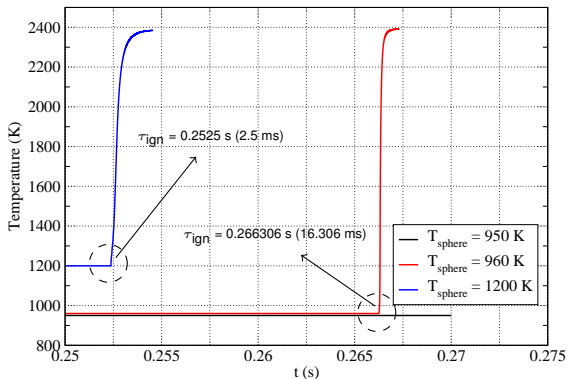
When does ignition take place ?



Temperature maximum in computational domain

$$\tau_{\text{ign}} = T_{\text{sphere}} + 150\text{K}$$

When does ignition take place ?



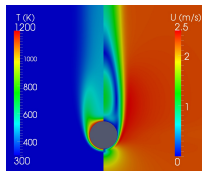
Temperature maximum in computational domain

$$\tau_{\text{ign}} = T_{\text{sphere}} + 150\text{K}$$

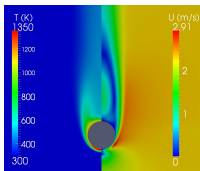
Where does ignition take place ? ^(1/8)

$T_{\text{sphere}} = 1200 \text{ K}$ - Ignition Evolution

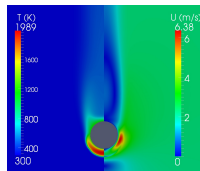
$t = 0.25237 \text{ s}$



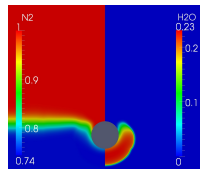
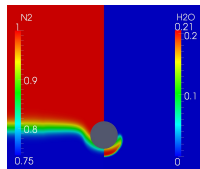
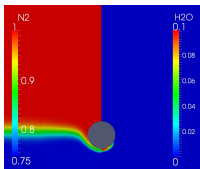
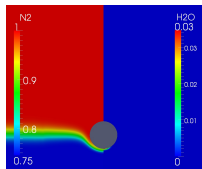
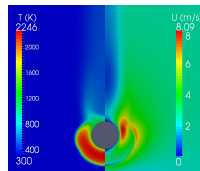
$t = 0.25250 \text{ s}$



$t = 0.25275 \text{ s}$



$t = 0.2530 \text{ s}$



Shortly before ignition

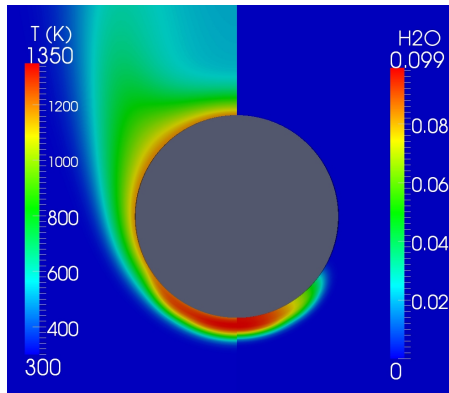
Ignition

Flame kernel formation

Flame propagation

Where does ignition take place ? (2/8)

$$T_{\text{sphere}} = 1200 \text{ K}$$

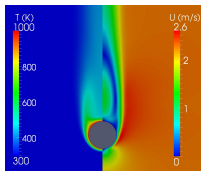


Closeup to ignition location - $\theta = 0^\circ$

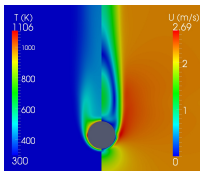
Where does ignition take place ? ^(3/8)

$T_{\text{sphere}} = 1000 \text{ K}$ - Ignition Evolution

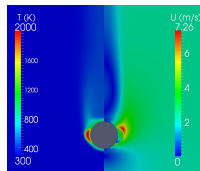
$t = 0.254354 \text{ s}$



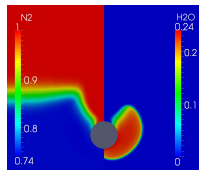
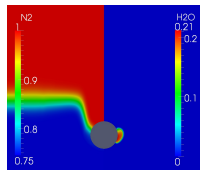
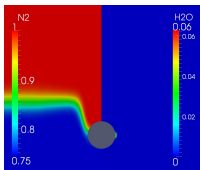
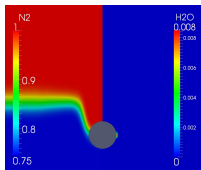
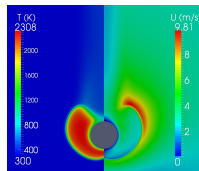
$t = 0.254386 \text{ s}$



$t = 0.254466 \text{ s}$



$t = 0.25475 \text{ s}$



Shortly before ignition

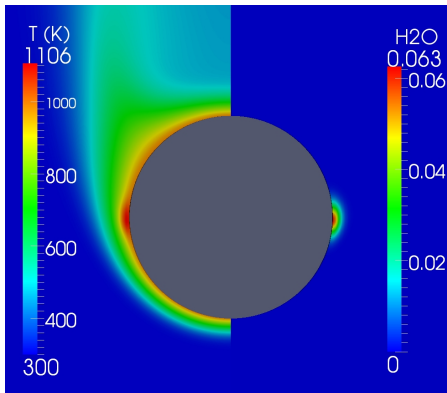
Ignition

Flame kernel formation

Flame propagation

Where does ignition take place ? ^(4/8)

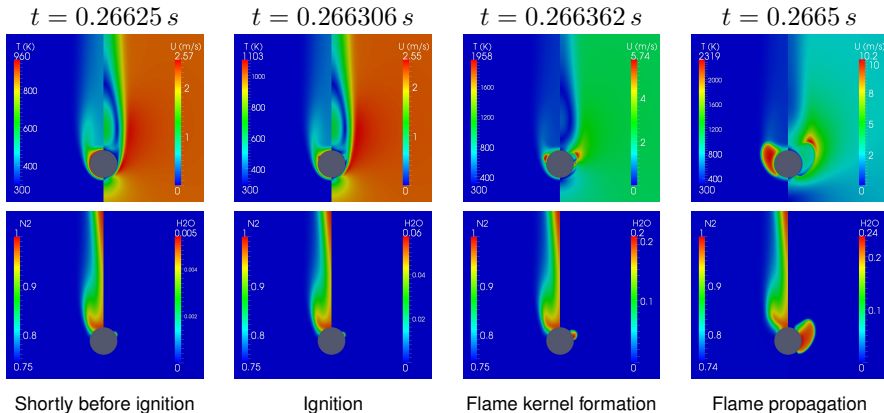
$$T_{\text{sphere}} = 1000 \text{ K}$$



Closeup to ignition location - $\theta = 90^\circ$

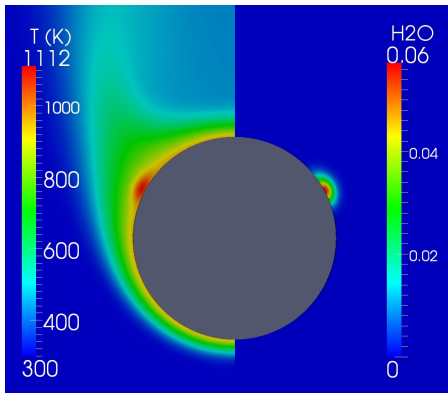
Where does ignition take place ? ^(5/8)

$T_{\text{sphere}} = 960 \text{ K}$ - Ignition Evolution



Where does ignition take place ? (6/8)

$$T_{\text{sphere}} = 960 \text{ K}$$

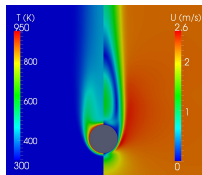


Closeup to ignition location - $\theta = 115^\circ$ (threshold)

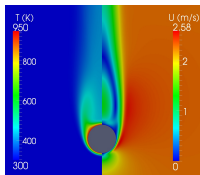
Where does ignition take place ? ^(7/8)

$T_{\text{sphere}} = 950 \text{ K}$ - No Ignition

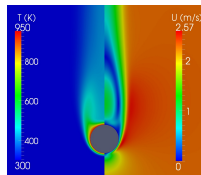
$t = 0.255 \text{ s}$



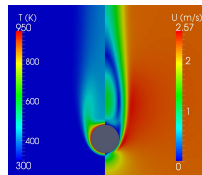
$t = 0.260 \text{ s}$



$t = 0.265 \text{ s}$

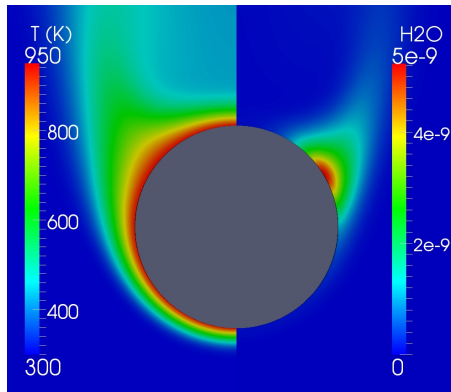


$t = 0.270 \text{ s}$



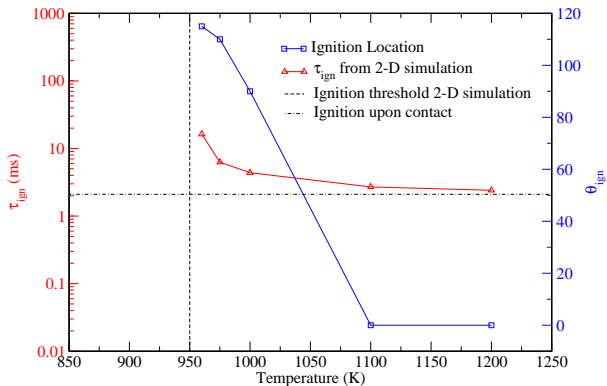
Where does ignition take place ? (8/8)

$$T_{\text{sphere}} = 950 \text{ K}$$



No Ignition

Results Summary

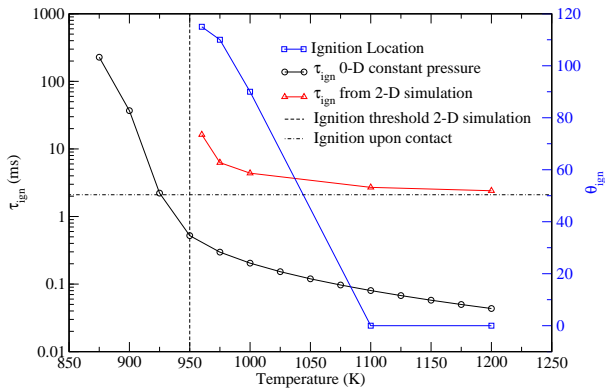


Ignition times and locations from 2D simulations

Outline

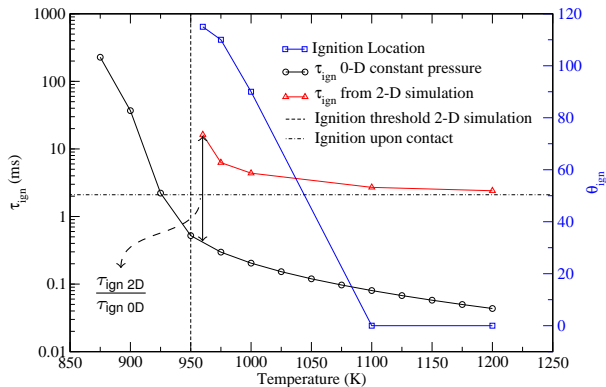
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Ignition times analysis



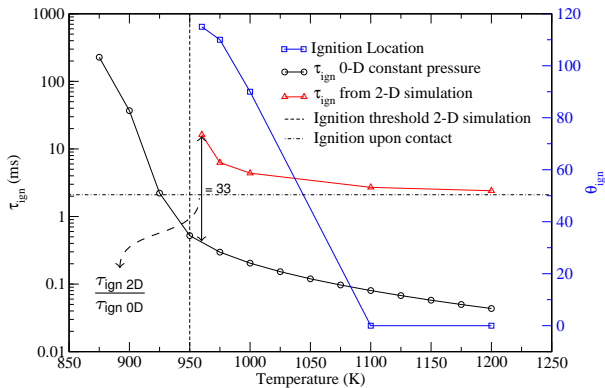
Comparison of 2D and constant pressure ignition times

Ignition times analysis



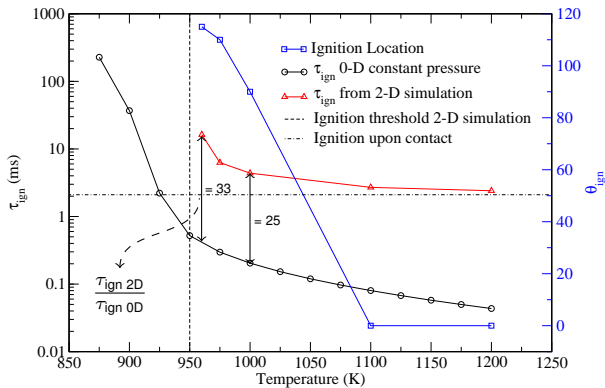
Comparison of 2D and constant pressure ignition times

Ignition times analysis



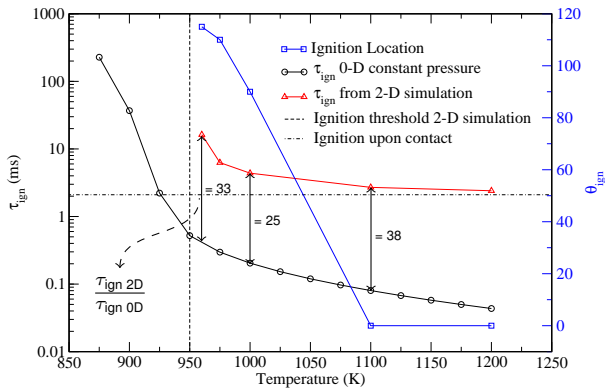
Comparison of 2D and constant pressure ignition times

Ignition times analysis



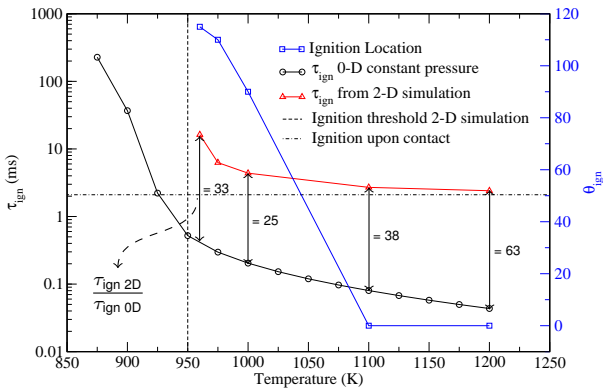
Comparison of 2D and constant pressure ignition times

Ignition times analysis



Comparison of 2D and constant pressure ignition times

Ignition times analysis



Comparison of 2D and constant pressure ignition times

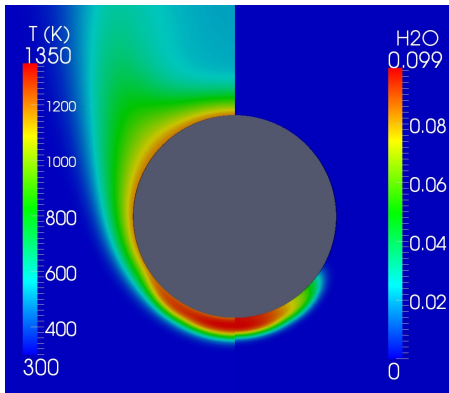
Energy equation analysis (1/5)

Recall the energy equation

$$\underbrace{\frac{\partial(\rho h)}{\partial t}}_{\text{Sum (---)}} = \underbrace{-\nabla \cdot (\rho \mathbf{u} h)}_{\text{hConvection (---)}} + \underbrace{\nabla \cdot (\kappa / c_p \nabla h)}_{\text{hDiffusion (---)}} + \underbrace{q_{chem}}_{\text{hSource (---)}}$$

Energy equation analysis (2/5)

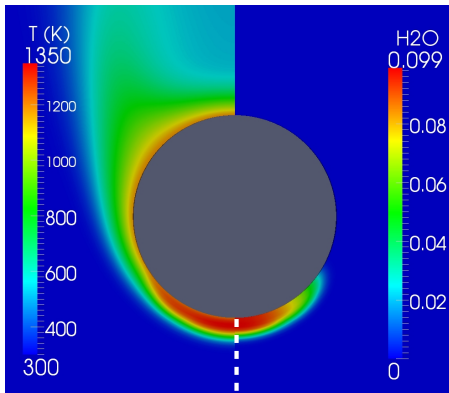
$$T_{\text{sphere}} = 1200 \text{ K}$$



Closeup to ignition location - $\theta = 0^\circ$

Energy equation analysis (2/5)

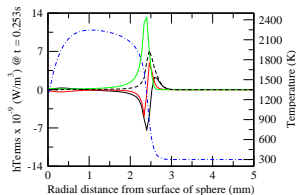
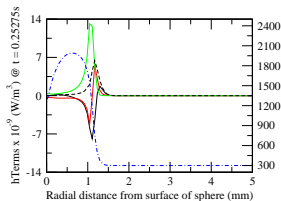
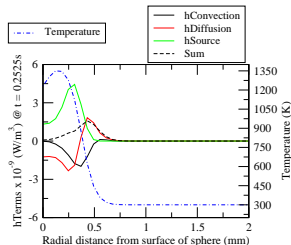
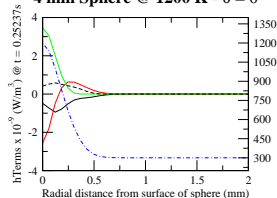
$$T_{\text{sphere}} = 1200 \text{ K}$$



Closeup to ignition location - $\theta = 0^\circ$

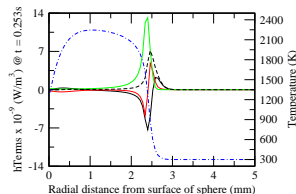
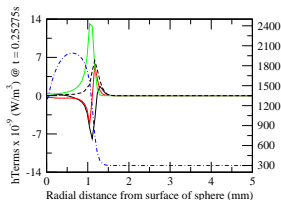
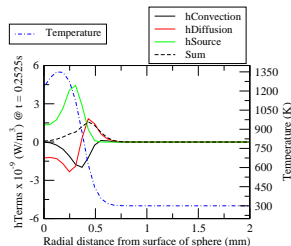
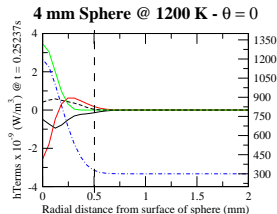
Energy equation analysis (3/5)

4 mm Sphere @ 1200 K - $\theta = 0$



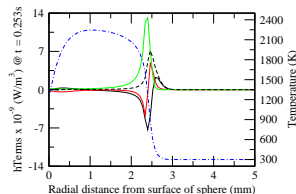
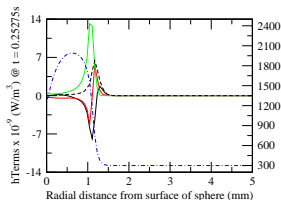
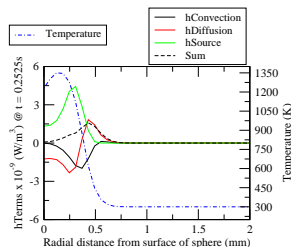
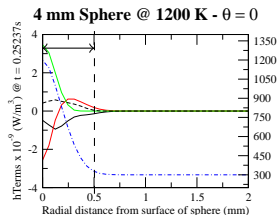
Contributions of each term in energy equation and temperature along radial distance from sphere's surface

Energy equation analysis (3/5)



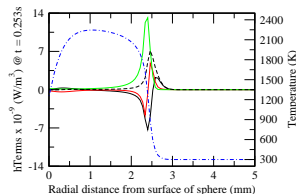
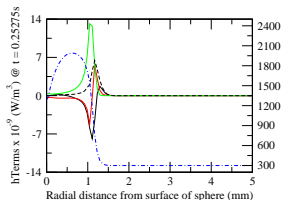
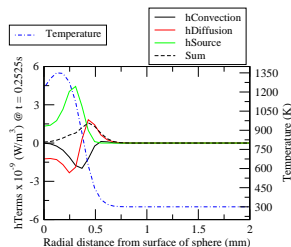
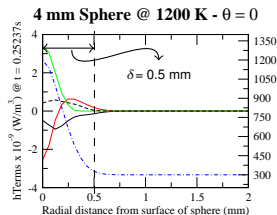
Contributions of each term in energy equation and temperature along radial distance from sphere's surface

Energy equation analysis (3/5)



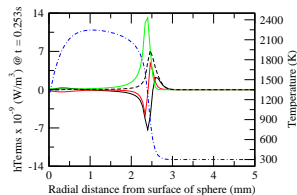
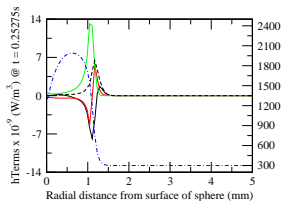
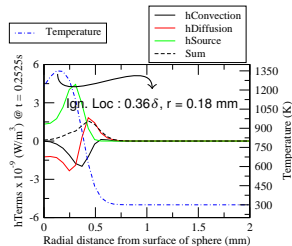
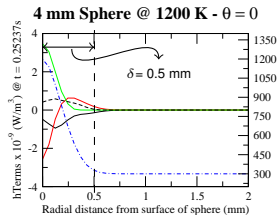
Contributions of each term in energy equation and temperature along radial distance from sphere's surface

Energy equation analysis (3/5)



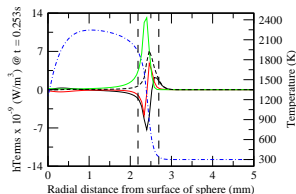
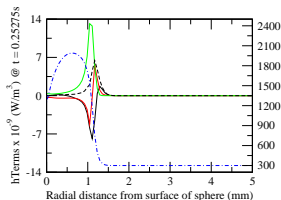
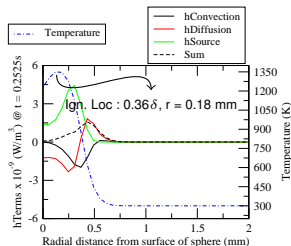
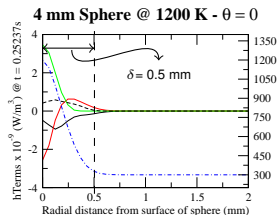
Contributions of each term in energy equation and temperature along radial distance from sphere's surface

Energy equation analysis (3/5)



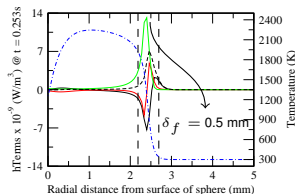
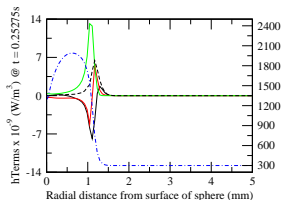
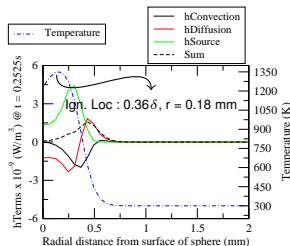
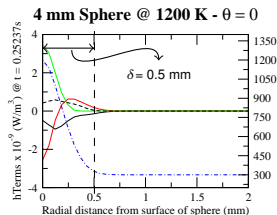
Contributions of each term in energy equation and temperature along radial distance from sphere's surface

Energy equation analysis (3/5)



Contributions of each term in energy equation and temperature along radial distance from sphere's surface

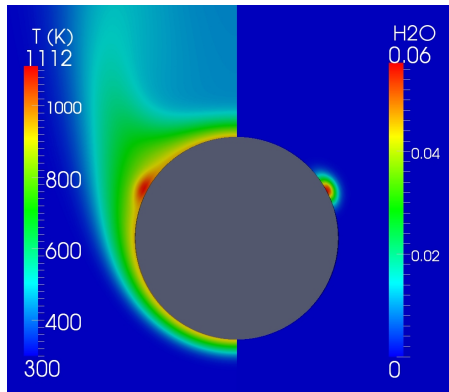
Energy equation analysis (3/5)



Contributions of each term in energy equation and temperature along radial distance from sphere's surface

Energy equation analysis (4/5)

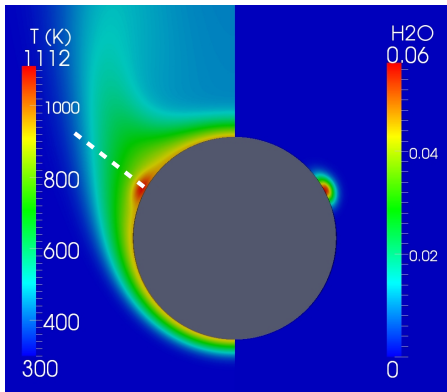
$$T_{\text{sphere}} = 960 \text{ K}$$



Closeup to ignition location - $\theta = 115^\circ$ (threshold)

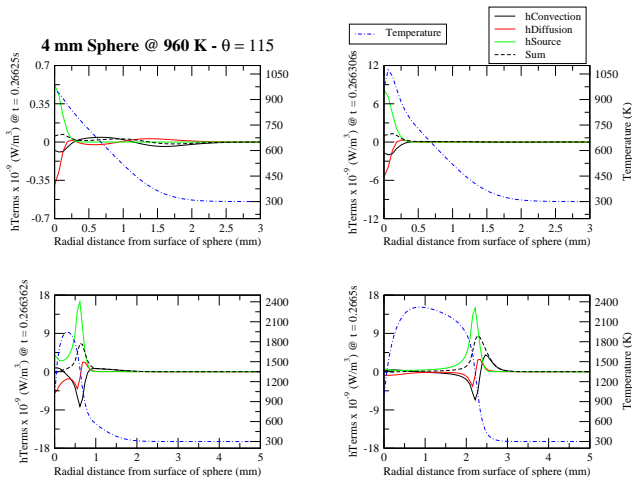
Energy equation analysis (4/5)

$$T_{\text{sphere}} = 960 \text{ K}$$



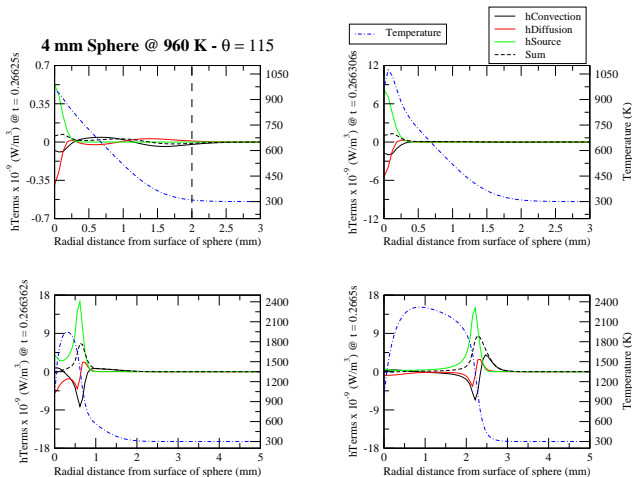
Closeup to ignition location - $\theta = 115^\circ$ (threshold)

Energy equation analysis (5/5)



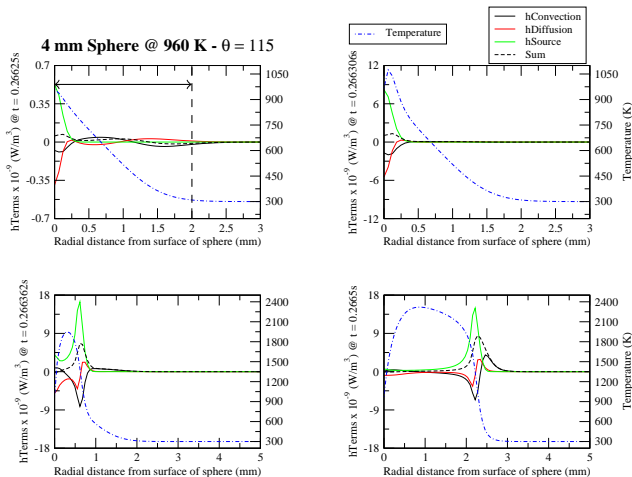
Contributions of each term in energy equation and temperature along radial distance from sphere's surface

Energy equation analysis (5/5)



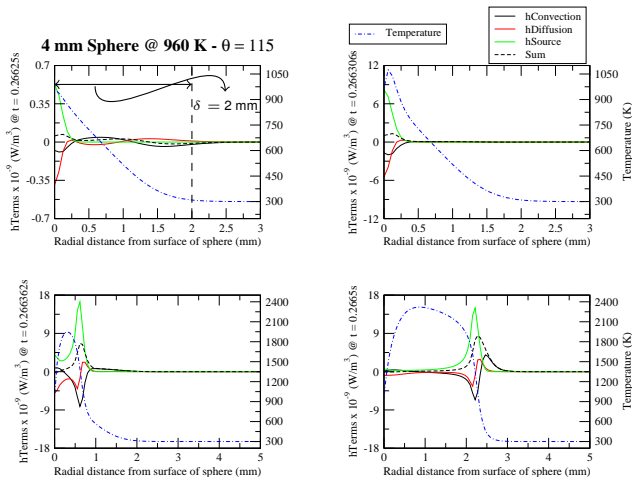
Contributions of each term in energy equation and temperature along radial distance from sphere's surface

Energy equation analysis (5/5)



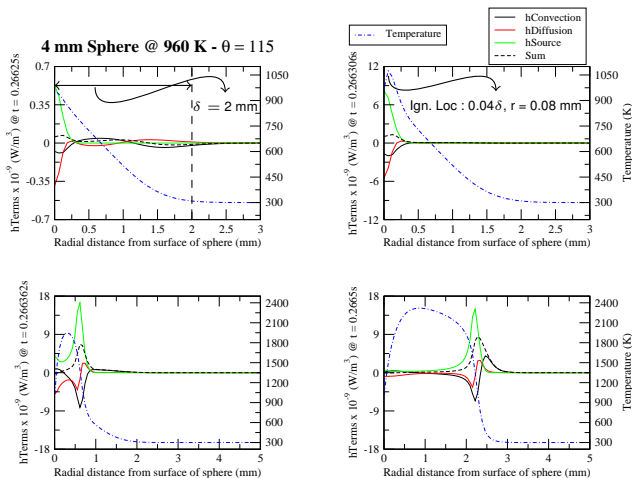
Contributions of each term in energy equation and temperature along radial distance from sphere's surface

Energy equation analysis (5/5)



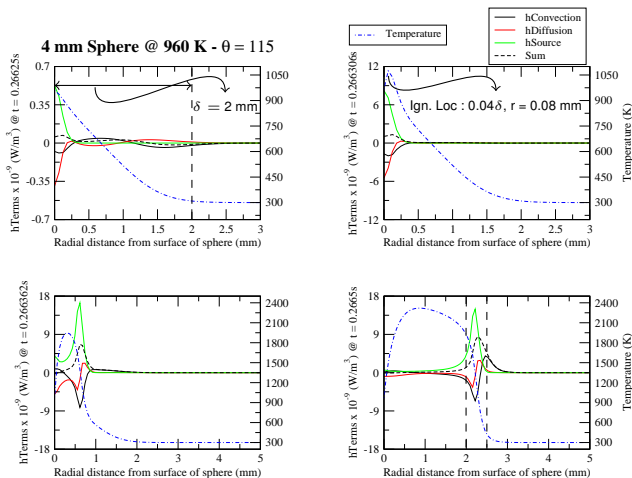
Contributions of each term in energy equation and temperature along radial distance from sphere's surface

Energy equation analysis (5/5)



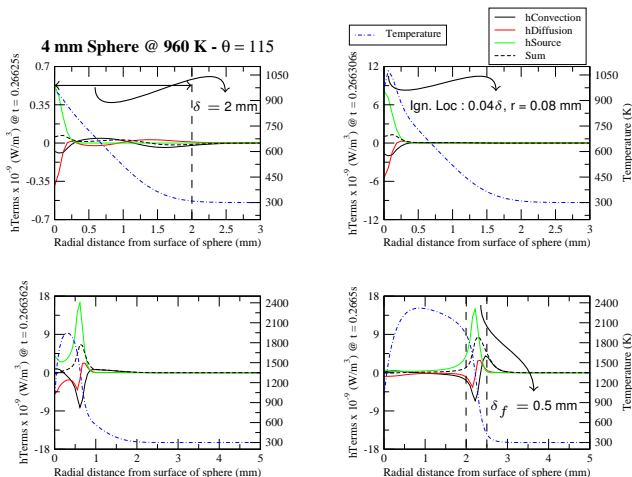
Contributions of each term in energy equation and temperature along radial distance from sphere's surface

Energy equation analysis (5/5)



Contributions of each term in energy equation and temperature along radial distance from sphere's surface

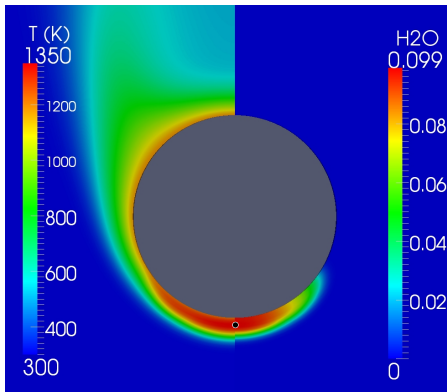
Energy equation analysis (5/5)



Contributions of each term in energy equation and temperature along radial distance from sphere's surface

Temporal evolution near ignition location ^(1/2)

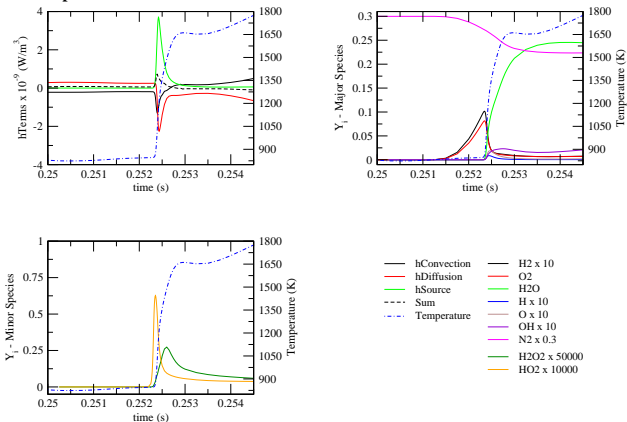
$$T_{\text{sphere}} = 1200 \text{ K}$$



Closeup to ignition location - $\theta = 0^\circ$

Temporal evolution near ignition location (2/2)

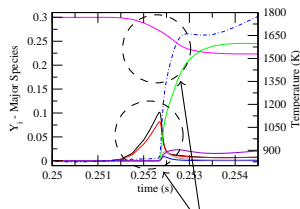
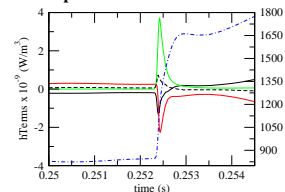
4 mm Sphere @ 1200 K - $\theta = 0$ @ 0.36 δ



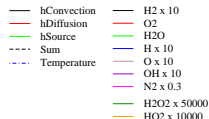
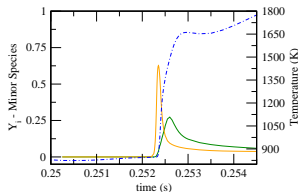
Temporal Evolution of each term in energy equation, temperature and species mass fractions at the ignition location

Temporal evolution near ignition location (2/2)

4 mm Sphere @ 1200 K - $\theta = 0$ @ 0.36 δ



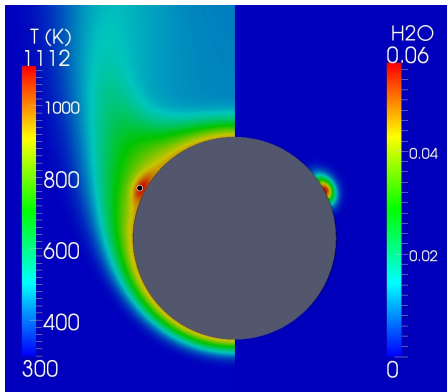
B.L. Flushing - Ignition occurs in more diluted mixture



Temporal Evolution of each term in energy equation, temperature and species mass fractions at the ignition location

Temporal evolution near ignition location (3/4)

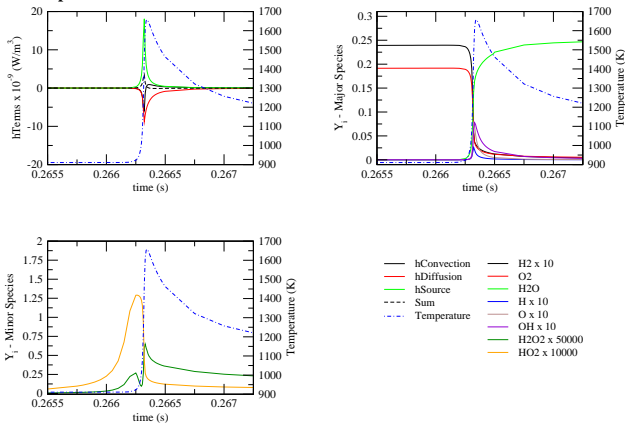
$$T_{\text{sphere}} = 960 \text{ K}$$



Closeup to ignition location - $\theta = 115^\circ$ (threshold)

Temporal evolution near ignition location (4/4)

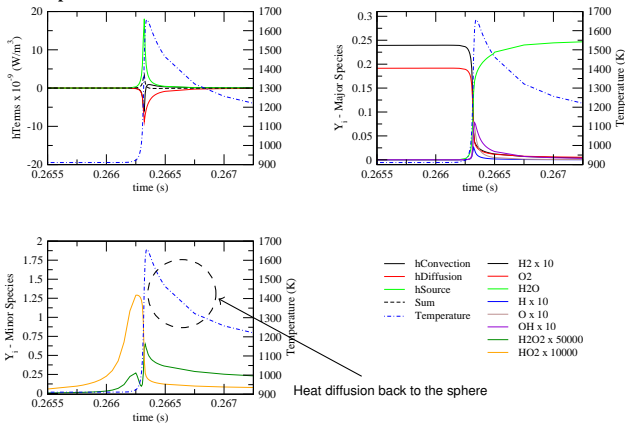
4 mm Sphere @ 960 K - $\theta = 115^\circ$ @ 0.048



Temporal Evolution of each term in energy equation, temperature and species mass fractions at the ignition location

Temporal evolution near ignition location (4/4)

4 mm Sphere @ 960 K - $\theta = 115^\circ$ @ 0.048

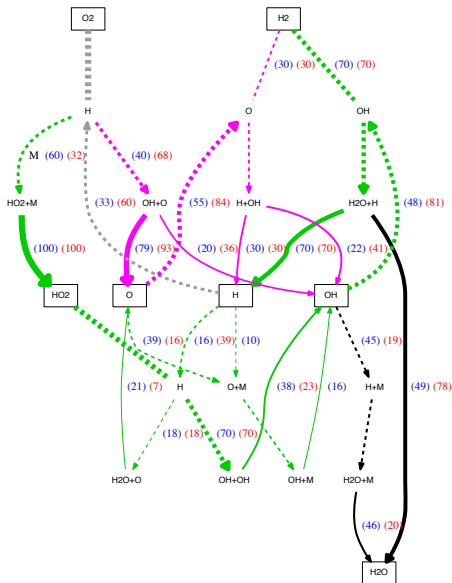


Temporal Evolution of each term in energy equation, temperature and species mass fractions at the ignition location

$$T_{\text{sphere}} = 960\text{K}$$

--- : Reservoir Outputs

: Non-chainbranching



Chemical Pathways

$T_{\text{sphere}} = 1200\text{K}$

$T_{\text{sphere}} = 960\text{K}$

Box : Species Reservoirs

— : Reservoir Inputs

--- : Reservoir Outputs

— : Chain-branching

— : Mixed pathways

— : Non-chainbranching

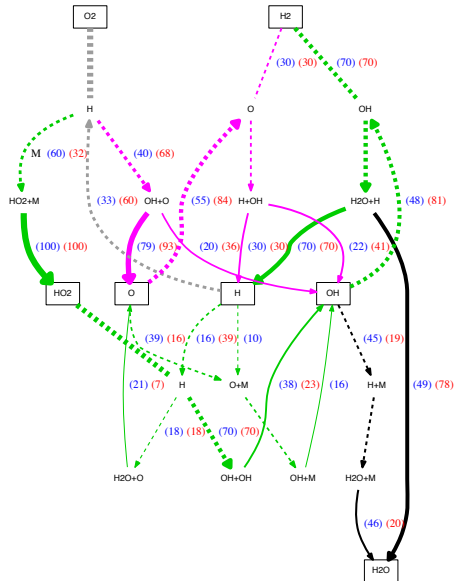
At high T :

OH radicals mostly produced by chain-branching processes (77%)

$R_1 : \text{O}_2 + \text{H} = \text{OH} + \text{O}$

$R_2 : \text{H}_2 + \text{O} = \text{H} + \text{OH}$

Non-chain branching through Path 1 (23%)



Chemical Pathways

$T_{\text{sphere}} = 1200\text{K}$

$T_{\text{sphere}} = 960\text{K}$

Box : Species Reservoirs

— : Reservoir Inputs

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Non-chain branching through Path 1 (23%)

At low T :

Chain-branching processes significantly less (42%)

Non-chain branching processes

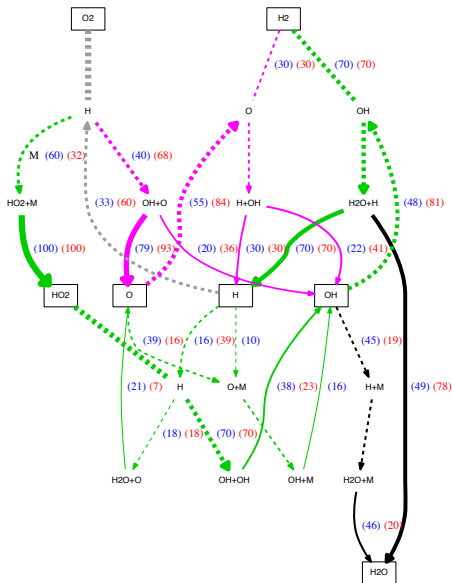
Path 1 (38%) :

$R_5 : \text{H} + \text{O}_2(+\text{M}) = \text{HO}_2(+\text{M})$

$R_3 : \text{HO}_2 + \text{H} = \text{OH} + \text{OH}$

Path 2 (16%) :

$R_6 : \text{H} + \text{O}(+\text{M}) = \text{OH}(+\text{M})$



Outline

- 1 Motivation
- 2 Previous Work
- 3 Goal
- 4 Physical Model, Numerical Approach and Simulation Parameters
- 5 Results
- 6 Discussion
- 7 Closing Remarks**

Closing Remarks (1/2)

- Quantitative prediction of ignition thresholds for hot surfaces require a detailed model that includes correct initial and boundary conditions to capture important features such as boundary layer separation, and energy transport processes
- Ignition occurs within the thermal boundary layer at a location that depends strongly on temperature
- Large differences observed between 2D and 0D ignition times suggests that simplified models based on comparison of residence times with ignition delay times are inappropriate
- As the temperature decreases to the ignition threshold, non-chain branching chemical pathways are favored over chain branching processes

Closing Remarks (2/2)

- Two distinct behaviors observed :
 - Far from the ignition threshold
 - Reaction starts shortly after contact with reactive mixture
 - Ignition occurs between the front stagnation point and separation region depending upon the sphere's surface temperature
 - Ignition time is very short and takes place in a more diluted mixture compared cases close to the ignition threshold
 - Closer to the threshold
 - Rate of heat deposition into the gas not high enough to trigger fuel conversion during transit from the front stagnation point to the separation region
 - Boundary layer separation results in a zone of slower moving gas, where reactive mixture is "confined", conduction of heat takes place readily and convective losses are minimal

Conclusion

Not only does flow separation play an important role in hot particle ignition,
but also when considering different geometries

